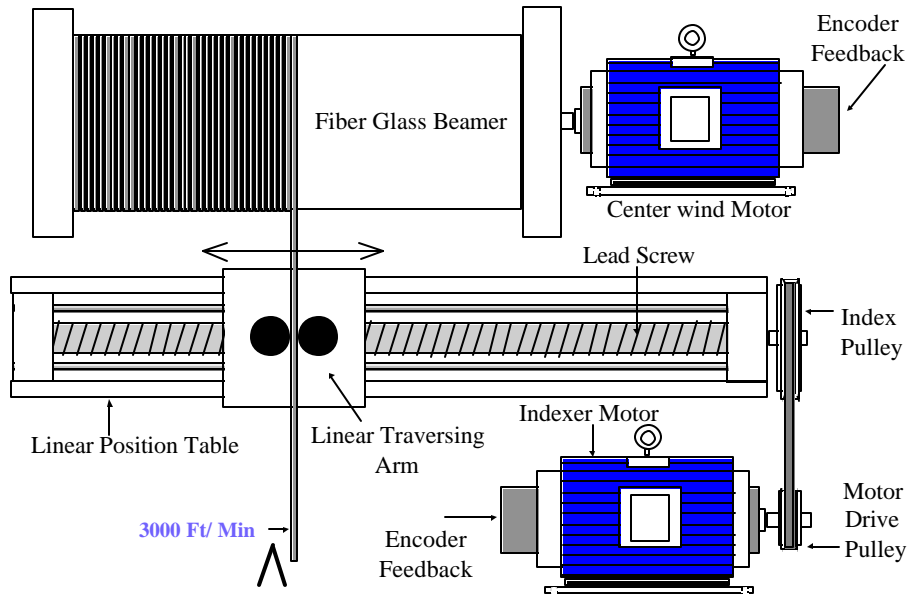


This form is used to help size common indexing applications. The form contains: Indexing overview, sizing example, and customer application data.



**Indexing** is a method of providing position and velocity control of a machine section or workpiece. Traditionally, Indexer control had been accomplished using stepper and servo controls. With the improvements of Flux Vector AC drives, which regulates the magnetic flux and torque generating current of induction motor, position and velocity control can be accomplished using the less costly Flux Vector drive.

The Servo or Vector drive controls the indexing motion by controlling the motor to move a predefined distance and velocity. An optical encoder or resolver is used to close the position and velocity loop during a move profile. The processor move command will be broken down into a specific number of pulses. During the move command, the encoder pulses provide feedback. By using **Custom Application Software**, the AC vector drive has the ability to count the number of pulses.

The predefined profiles are stored in the software <sup>1</sup>, and the following parameters can be programmed.

<sup>1</sup> For GPD 515 using Custom Software, The version G5 + source code is required.

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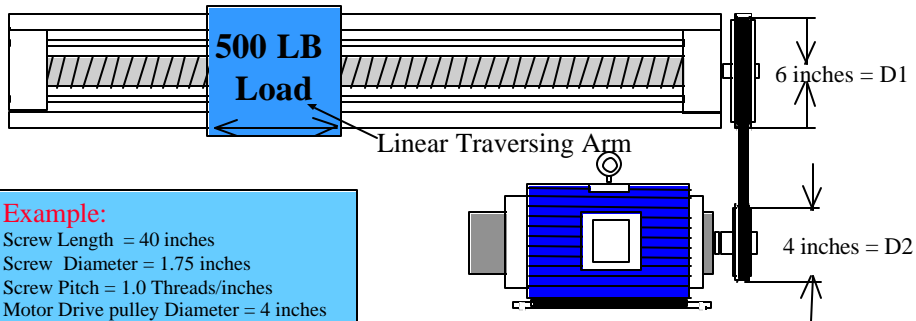
<u>Parameters</u>	<u>Communication Control</u>
Speed1, Home speed	Modbus
Preset Speed 1,2,3	Modbus-Plus
Acceleration	RS232-RS485
Deceleration	Profibus
Distance	Interbus
Dwell	
Home sequence	

**Motion System Performance Comparison**

<u>Type</u>	<u>V/f Control</u>	<u>Vector Control</u>	<u>AC Servo</u>
HP Range	0.5- 1500 HP	0.5-1500HP	1-100 HP
Speed Range control	40:1	1000:1	200,000:1
Speed control accuracy	± 2%	± .01%	± .01%
Frequency control	1- 400 Hz	1- 400 Hz	1- 400 Hz
Torque Range		.01-150%	.01-200%
Torque Control	No	Yes	Yes
Velocity control	No	Yes	Yes
Positioning	No	Yes	Yes
Repeatability	Not Possible		± 1 arcmin
Motor Inertia:Load Intertia	N/A		10:1-200:1

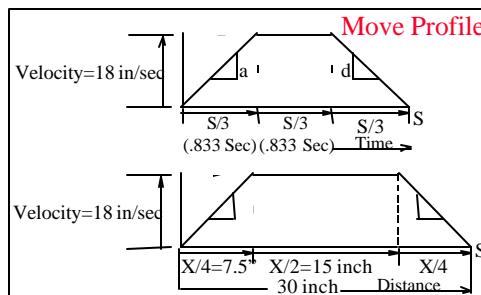
The application below requires calculations that are found on the next page. There are many different sizing programs in the market, but without having the basic understanding of the calculations, a critical profile or mechanical question could be missed.

The calculations require a few assumptions. The velocity & distance profiles are broken up into 3 sections. If you make the assumption that distance is  $x/4$  ( $x$  is distance) for acceleration & deceleration, and  $x/2$  for constant velocity, the Time profiles can be broken into  $s/3$  sections ( $s$  is time). The profiles are given in the **Move Profile** below.



**Example:**  
 Screw Length = 40 inches  
 Screw Diameter = 1.75 inches  
 Screw Pitch = 1.0 Threads/inches  
 Motor Drive pulley Diameter = 4 inches  
 Index table pulley Diameter = 6 inches  
 W1 = Weight Load pulley=4 lb  
 W2 =Weight Motor Pulley = 9lb  
 Motion requirement = 30 Inches  
 Speed requirement = 2.5 seconds;  
 Distance  $X/4= a=d$  & Distance  $X/2$  Run

- a = -d = Acceleration = \_\_\_\_\_ in/sec<sup>2</sup>
- v = Velocity = \_\_\_\_\_ in/sec
- p = Screw pitch \_\_\_\_\_ Threads/Inch
- DS = Screw Diameter \_\_\_\_\_ inches
- W = Load \_\_\_\_\_ LBS
- F = Breakaway Force \_\_\_\_\_ LBS
- e = Efficiency of screw \_\_\_\_\_ %
- L=Length of Screw \_\_\_\_\_ Inches
- J = inertia \_\_\_\_\_ oz-in<sup>2</sup>
- D1 = Dia Load pulley \_\_\_\_\_ inches
- D2 = Dia Motor Pulley \_\_\_\_\_ inches
- W1 = Weight Load pulley \_\_\_\_\_ 4 \_\_\_\_\_ lb
- W2 =Weight Motor Pulley \_\_\_\_\_ 9 \_\_\_\_\_ lb



**Formula**

**Sizing Example**

$$\text{Acceleration} = a = -d = \frac{2X}{t^2} = \frac{2(X/4)}{(S/3)^2} = \frac{4.5X}{S^2}$$

**Steps** ①  $a = -d = \frac{4.5X}{S^2} = \frac{4.5 * 30}{2.5^2} = 21.6 \text{ in/sec}^2$

$$\text{Velocity} = at = \frac{4.5X}{S^2} * \frac{S}{3} = \frac{1.5X}{S}$$

②  $v = at = 1.5 (30 \text{ inch})/2.5 \text{ Sec} = 18 \text{ inch / Sec}$   
 $18 \text{ in/sec} * 6 \text{ in} * 60 \text{ sec}$

$$\text{Max RPM}_{\text{motor}} = \frac{\text{Max Speed} * \text{Lead Screw Pulley Dia} * (60 \text{ sec})}{\text{Pitch Dia} * \text{Motor Pulley Dia} * (\text{min})}$$

③  $\text{RPM}_{\text{motor}} = \frac{18 \text{ in/sec} * 6 \text{ in} * 60 \text{ sec}}{1 \text{ in/rev} * 4 \text{ in} * \text{min}} = 1620 \text{ RPM}$

$$\text{Torque}_{\text{total}} = (\text{Torque}_{\text{Friction}} + \text{Torque}_{\text{Acceleration}} \text{ oz - in}) 1.10$$

④  $F = \text{Force}_{\text{Friction}} = .25 * 500 \text{ lb} * 16 \text{ oz/lb} = 2000 \text{ oz}$

$$\text{Torque}_{\text{Friction}} = \frac{E(D2/D1)}{2\pi * p * e} \quad \& \quad F = \text{Force}_{\text{Friction}} = u_s * W$$

⑤  $\text{Torque}_{\text{Friction}} = \frac{(4/6) 2000 \text{ oz}}{2\pi * 1.0 \text{ threads/in} * .65} = 326 \text{ oz-in}$

$$J_{\text{Load @ motor}} = \frac{W(D2/D1)^2}{(2\pi p)^2}$$

⑥  $J_{\text{Load @ m}} = \frac{500 \text{ lb} * 16 \text{ oz/lb} * (4/6)^2}{(2\pi * 1.0 \text{ threads/in})^2} = 90.15 \text{ oz-in}^2$

$$J_{\text{lead screw @ motor}} = \frac{\pi L^2 R^4 (D2/D1)^2}{2} ; \quad ? = \text{Steel density} = 4.48 \text{ oz/in}^3$$

⑦  $J_{\text{lead screw @ m}} = \frac{\pi * 40 \text{ in}^4 * 4.48 \text{ oz/in}^3 * (1.75 \text{ in}/2)^4 * (4/6)^2}{2} = 73.29 \text{ oz - in}^2$

$$\text{load pulley @ motor} = \frac{W_{\text{load Pulley}} R_{\text{load Pulley}}^2}{2} * (D2/D1)^2$$

⑧  $J_{\text{load p @ motor}} = \frac{9 \text{ lb} * 16 \text{ oz/lb} * 3^2 * (4/6)^2}{2} = 288 \text{ oz-in}^2$

$$\text{Motor Pulley @ motor} = \frac{W_{\text{Motor Pulley}} * R_{\text{load Pulley}}^2}{2}$$

⑨  $J_{\text{Motor Pulley @ motor}} = \frac{6 \text{ lb} * 16 \text{ oz/lb} * 3^2}{2} = 432 \text{ oz-in}^2$

$$\omega_{\text{motor}} = 2\pi * p * \text{velocity} @ t = .833 \text{ sec} * (D1/D2) = \text{angular velocity}$$

⑩  $\omega_{\text{motor}} = 2\pi * 1.0 \text{ thread/in} * 18 \text{ in/sec} * (6/4)$

$$\text{Motor @ 1.5hp given in Marathon catalog} = 0.14 \text{ lb-ft}^2$$

⑪  $J_{\text{Motor}} = 0.14 \text{ lb-ft}^2 * 16.0 \text{ oz/lb} * (12 \text{ in}/1 \text{ ft})^2 = 322.56 \text{ oz-in}^2$   
 $= 169.56 \text{ radians/sec}$

$$I_{\text{Accel}} = \frac{? (J_{\text{load}}/e + J_{\text{lead screw}} + J_{\text{load pulley}} + J_{\text{Motor Pulley}} + J_{\text{Motor}})}{g t}$$

⑫  $T_{\text{Accel}} = \frac{169.56 (90.15 / .65 + 73.29 + 288 + 432 + 322.56)}{386 \text{ in/sec}^2 * .833} = 661 \text{ oz-in}$

$$\text{orque}_{\text{total}} = (\text{Torque}_{\text{Friction}} + \text{Torque}_{\text{Acceleration}} \text{ oz - in}) 1.10$$

⑬  $\text{Torque}_{\text{total}} = (326 \text{ oz-in} + 661 \text{ oz-in}) 1.10 = 1085 \text{ oz-in}$

$$\text{HP} = \frac{\text{Torque}_{\text{total}} * (\text{RPM max})}{5252 * 12 \text{ in/lb} * 12 \text{ in/ft}}$$

⑭  $\text{HP} = \frac{1085 \text{ oz-in} * (1620 \text{ RPM})}{5252 * 16 \text{ oz/lb} * 12 \text{ in/ft}} = 1.75 \text{ HP}$

**Customer Data**

Company Name	<input type="checkbox"/> End user <input type="checkbox"/> Distributor <input type="checkbox"/> OEM
Contact Name #1	Contact Name #1 e-mail
Contact Name #2	Contact Name #2 e-mail
Address	City
State	Zip
Phone	Fax

**Machine Data**

Type of application (Lead Screw, Conveyer, Rack and pinion, Turntable, Machine tool) \_\_\_\_\_

Material moved \_\_\_\_\_

p = Screw pitch            \_\_\_\_\_ Threads/Inch

DS = Screw Diameter    \_\_\_\_\_ inches

W = Load                    \_\_\_\_\_ LBS

F = Breakaway Force    \_\_\_\_\_ LBS

e = Efficiency of screw    \_\_\_\_\_ %

L=Length of Screw        \_\_\_\_\_ Inches

J = inertia                    \_\_\_\_\_ oz-in<sup>2</sup>

**Transmission Data, Pulley or chain and sprocket**

D1 = Diameter Load pulley or sprocket    \_\_\_\_\_ inches

D2 = Diameter Motor Pulley or sprocket    \_\_\_\_\_ inches

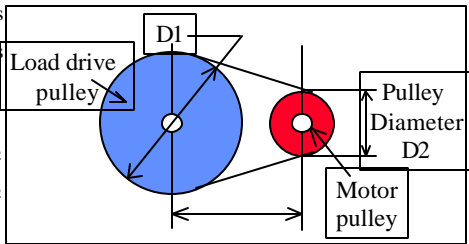
W1 = Weight Load pulley or sprocket        \_\_\_\_\_ lb

W2 =Weight Motor Pulley or sprocket        \_\_\_\_\_ lb

Inertia of Pulley or sprocket #1<sup>A</sup>            \_\_\_\_\_ oz-in<sup>2</sup>

Inertia of Pulley or sprocket #2<sup>A</sup>            \_\_\_\_\_ oz-in<sup>2</sup>

Efficiency    \_\_\_\_\_ %



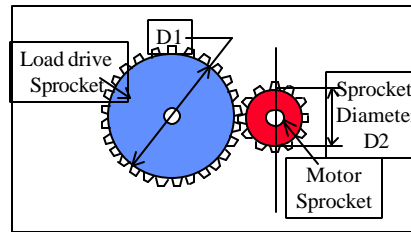
<sup>A</sup> If not known, then review example above

**Gear Box**

Gear Box ratio \_\_\_\_\_ Motor: Load  
 Inertia of Gear Box<sup>B</sup> \_\_\_\_\_ oz-in<sup>2</sup>  
 Efficiency \_\_\_\_\_ %

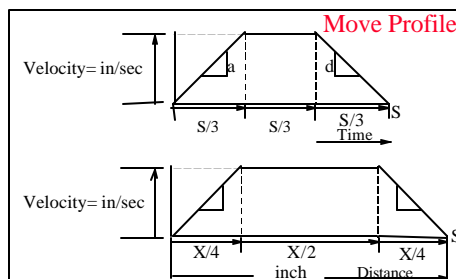
**Gears**

D1 = Diameter Load Gear \_\_\_\_\_ inches  
 D2 = Diameter Motor Gear \_\_\_\_\_ inches  
 Number of teeth Load Gear \_\_\_\_\_ teeth  
 Number of teeth Motor Gear \_\_\_\_\_ teeth  
 W1 = Weight Load pulley Gear \_\_\_\_\_ lb  
 W2 =Weight Motor Gear \_\_\_\_\_ lb  
 Inertia of Gear<sup>A</sup> \_\_\_\_\_ oz-in<sup>2</sup>  
 Inertia of Gear<sup>A</sup> \_\_\_\_\_ oz-in<sup>2</sup>  
 Efficiency \_\_\_\_\_ %



**Move Profile**

a = -d = Acceleration = \_\_\_\_\_ in/sec<sup>2</sup> If Acceleration = Deceleration (90% of Applications)  
 Acceleration = \_\_\_\_\_ in/sec<sup>2</sup> If Acceleration ≠ Deceleration  
 Deceleration = \_\_\_\_\_ in/sec<sup>2</sup> If Acceleration ≠ Deceleration  
 Machine Design speed \_\_\_\_\_ (Inches/ Seconds)  
 Minimum move profile \_\_\_\_\_ seconds



<sup>A</sup> If not known, then review example above

**Drive Data**

Manufacture \_\_\_\_\_ Model # \_\_\_\_\_  
 Horse Power \_\_\_\_\_  
 Winder Drive  New Application  Retrofit  
 Existing Voltage  230VAC  460VAC  575VAC  
 Existing Drive system  AC drive  DC drive

**Existing Motor Data**

Existing motor Manufacture \_\_\_\_\_ Model # \_\_\_\_\_  
 New motor required  Yes  No  
 Existing motor full load ratings: \_\_\_\_\_ AMPS  
 \_\_\_\_\_ Volt  
 \_\_\_\_\_ RPM (850, 1150, 1750)  
 Conduit Box location ( *if motor is to be replaced* )  F1  F2  F3 or  NA  
 Existing Blower Motor. \_\_\_\_\_ Voltage, \_\_\_\_\_ Amps or  NA  
 Existing Encoder Manufacture \_\_\_\_\_  NA  
  
 Existing Encoder  Digital  Analog AC  Absolute  Analog DC  
 Existing Encoder Manufacturer. \_\_\_\_\_  NA  
 Resolution Existing Encoder (PPR) \_\_\_\_\_ OR Volts/RPM \_\_\_\_\_  
 Encoder Pickup  Optical  Magnetic pickup

**Drive Enclosure information**

Ambient Temperature in control room \_\_\_\_\_ °F or \_\_\_\_\_ °C  
 Existing Drive Enclosure  NEMA 1  NEMA 12  NEMA 4X  AIR CONDITIONING  
 New Enclosure Spec  NEMA 1  NEMA 12  NEMA 4X  AIR CONDITIONING  
 Enclosure options  Duplex outlet  Lights  Empty cabinet for future use  
 Other \_\_\_\_\_

### Existing Power Distribution<sup>4</sup>

- Isolation Transformer \_\_\_\_ KVA Primary Voltage \_\_\_\_\_ AC Secondary voltage \_\_\_\_\_ AC
- Line Reactors Impedance \_\_\_\_\_ (%)  Load Reactors Impedance \_\_\_\_\_ (%)
- Dynamic Braking Resistor: Duty Cycle i.e. 3%, 5% \_\_\_\_\_ % Resistance \_\_\_\_\_ Ohms  
Dynamic Resistor Power rating \_\_\_\_\_ Watts

### Drive Communication Requirements

- Modbus Plus  Modbus  Device Net  Profibus  Arcnet LAN  Other \_\_\_\_\_

### Drive Input Requirements

- Start  Stop  Forward  Reverse  Run
- Jog  Preset Speed1  Preset Speed 2
- Other \_\_\_\_\_

### Drive Output Requirements

- Drive alarm fault  Drive severe fault  Run  Zero speed
- At speed  Encoder feedback pass through (PGX card)
- Other \_\_\_\_\_

**Comment [mkm1]:** May need Analog output to replace the individual pump pressure sensors.

### Analog Input

- speed reference  0-10VDC  4-20ma  Other \_\_\_\_\_

### Analog Output

- Drive Speed (Ft/minute)  Bus Voltage  Other \_\_\_\_\_

### Special Types of Control

- Drive system start  Drive system stop  Regenerative to fast stop - full current limit or ramped
- DC Bus Over Voltage Suppression (Used to prevent overvoltage tripping from an unbalanced load)
- Other \_\_\_\_\_

<sup>4</sup> The existing power distribution is required if Yaskawa is providing a drive system